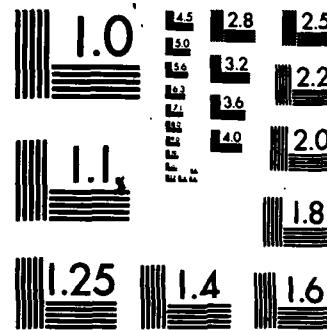


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COMPUTATION OF CURRENT-VOLTAGE-
CHARACTERISTICS IN A SEMICONDUCTOR
DEVICE USING ARC-LENGTH CONTINUATION

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COMPUTATION OF CURRENT-VOLTAGE-CHARACTERISTICS IN A SEMICONDUCTOR
DEVICE USING ARC-LENGTH CONTINUATION

Peter A. Markowich^{*1}, Christian A. Ringhofer¹, and Alois Steindl^{*}

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ABSTRACT

This paper is concerned with the computation of semiconductor device current-voltage characteristics. We describe an algorithm which allows the computation of characteristics by continuation in a parameter which approximates the arclength of the characteristic. The use of this parameterization allows the characteristic to continue beyond snap-back-voltages, while continuation in the voltage fails past snap-back-voltages. We discuss the implementation of the parameterization and give a numerical example.

AMS (MOS) Subject Classifications: 35B30, 35P30

Key Words: Semiconductor devices, Characteristics, Continuation, Newton's method

Work Unit Number 3 (Numerical Analysis and Scientific Computing)

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SIGNIFICANCE AND EXPLANATION

In this paper we present an algorithm for the numerical computation of current-voltage-characteristics in a semiconductor device (i.e. curves describing the dependence of the output current on the input voltage at some contacts). For certain devices (e.g. thyristors) the set of equations describing the state of the semiconductor device have multiple solutions for specific voltage ranges and snap-back phenomena occur (i.e. the current is not a single valued function of the voltage). This implies that the characteristic cannot be computed numerically by merely stepping up the voltage. Our algorithm involves reparameterizing the characteristic curve by means of a parameter which approximates the arclength of the curve. Continuation in this parameter past snap-back-points does not cause serious difficulty.

The authors
We discuss the implementation of the reparameterization and present a numerical example.

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COMPUTATION OF CURRENT-VOLTAGE-CHARACTERISTICS IN A SEMICONDUCTOR DEVICE

USING ARC-LENGTH CONTINUATION

Peter A. Markowich^{*,1}, Christian A. Ringhofer¹, and Alois Steindl^{*}

1. Introduction

The computation of static current-voltage characteristics for devices which exhibit snap-back phenomena (like thyristors or even a pn-junction in the avalanche case) has created problems since continuation in the voltage does not work beyond snap-voltages. Figure 1 shows a typical characteristic of a thyristor in forward bias with the snap-back voltages U_{S_1} and U_{S_2} .

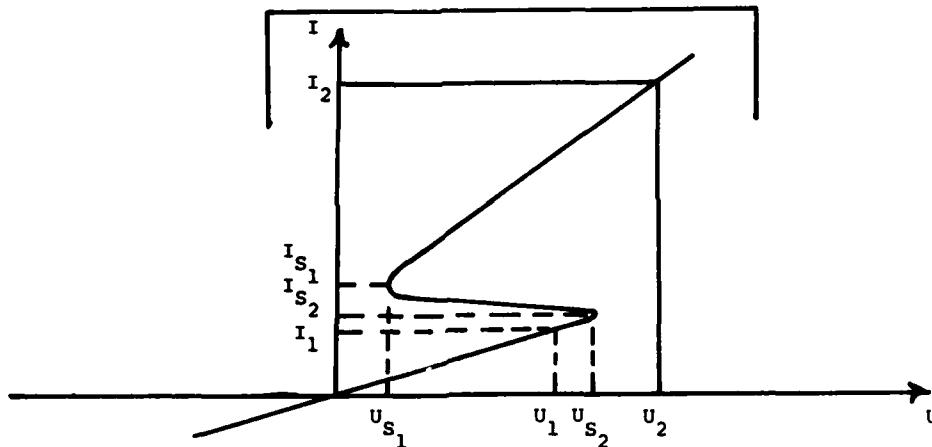


Figure 1. Current Voltage Characteristic of a Thyristor.

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Assume that the point (U_1, I_1) was computed (say by starting at $(0,0)$) and by gradually stepping up the voltage by the increment ΔU). Then, if $U_2 = U_1 + \Delta U > U_{S_2}$, the point (U_2, I_2) already lies on the upper branch of the characteristic and Newton's method for the numerical computation of (U_2, I_2) will probably fail when providing an initial guess which is computed just by using the previously computed solutions. The (dynamically stable) upper branch emerging from (U_{S_1}, I_{S_1}) cannot be computed by continuation in U starting from some point on the (also dynamically stable) 'lower branch' connecting $(0,0)$ and (U_{S_2}, I_{S_2}) .

In this paper we demonstrate how to avoid this problem by introducing an arclength-type parameter. The characteristic can be computed past snap-back voltages when doing continuation in this new parameter. This procedure is well known to mathematicians, however, most semiconductor-device simulation codes do not make use of it yet.

We also demonstrate how an already existing code, which solves the fundamental semiconductor device equations for given contact voltages has to be augmented to accommodate the reparameterization. The augmentation turns out to be very cheap in programming as well as in computer resources.

Finally we present numerical results for a one-dimensional pn-junction in the avalanche case.

2. Statement of the Problem

The basic static semiconductor device equations as given by Van Roosbroeck (1950) are

$$(2.1) \quad \operatorname{div}(eV\psi) = n - p - C \\ (2.2) \quad \operatorname{div}(D_n \nabla n - \mu_n n \nabla \psi) = R \\ (2.3) \quad \operatorname{div}(D_p \nabla p + \mu_p p \nabla \psi) = R \quad \left. \begin{array}{l} x \in \Omega \subset \mathbb{R}^n, n = 1, 2 \text{ or } 3. \end{array} \right\}$$

(We employ the usual notation) where Ω represents the device geometry. The electron and hole current densities are given by

$$(2.4) \quad J_n = q(D_n \nabla n - \mu_n n \nabla \psi),$$

$$(2.5) \quad J_p = -q(D_p \nabla p + \mu_p p \nabla \psi)$$

and the total current density

$$(2.6) \quad J = J_n + J_p.$$

For an MOS-device Laplace's equation

$$(2.7) \quad \operatorname{div}(eV\psi) = 0, \quad x \in \phi$$

holds where ϕ represents the oxide. The potential and the electrical displacement are assumed to be continuous at the interface $\partial\Omega_{0s} = \partial\Omega \cap \partial\phi$ and electrons and holes are not allowed to penetrate the oxide (n and p vanish in ϕ). We assume that the device has r contacts C_1, \dots, C_r . At these contacts the boundary conditions

$$(2.8) \quad \psi|_{C_i} = \tilde{\psi} + u_i$$

are prescribed where $\tilde{\psi}$ denotes the built in potential at the contact if C_i is Ohmic, the negative flat-band voltage if C_i is a gate contact on the metal-semiconductor interface. Mark function if C_i is a Schottky contact. u_i is the potential applied to C_i .

Also n and p are prescribed at Ohmic and Schottky contacts.

The remaining part of the boundary of the device is assumed to be insulating, that means the derivatives of ψ , n and p in normal direction to the boundary vanish there.

The outflow current density of C_i is given by

$$(2.9) \quad I_i = \int_{C_i} J \cdot n ds ,$$

where n denotes the exterior unit normal vector to C_i .

For the following we write the problem (2.1)-(2.3) (and (2.7) for a MOS device) subject to the mentioned boundary conditions (and interface condition for a MOS device) or a scaled version of it in operator form:

$$(2.10) \quad A(z, U_1, \dots, U_r) = 0, \quad z = (\psi, n, p)$$

while

$$(2.11) \quad A : Z \times \mathbb{R}^r \rightarrow Y$$

where Z and Y are appropriate (Banach) spaces of functions. In the sequel we are interested in the determination of the outflow current I_i for varying contact voltage $U_j \in \mathbb{R}$ and fixed voltages $U_1, \dots, U_{j-1}, U_{j+1}, \dots, U_r$. For notational simplicity we set $U := U_i$, $I := I_i$. We assume that the resulting current-voltage ($I-U$)-characteristic is a smooth curve in \mathbb{R}^2 which can be parameterized as follows

$$(2.12) \quad U = U(s), \quad I = I(s)$$

where

$$(2.13) \quad \dot{U}^2(s) + \dot{I}^2(s) = 1 \quad (\cdot \text{ denotes } \frac{d}{ds}) .$$

Then $s - s_0$ is the length of the arc connecting $(U(s_0), I(s_0))$ and $(U(s), I(s))$.

The goal of the analysis following this section is to facilitate the numerical computation of the curve (2.12). For further notational simplicity we denote

$$(2.14) \quad B(z, U) = A(z, U_1, \dots, U_{j-1}, U, U_{j+1}, \dots, U_r)$$

(all contact voltages except $U_j = U$ are fixed) where

$$(2.15) \quad B : Z \times \mathbb{R} \rightarrow Y .$$

3. Parameterization

The arclength parameterization (2.13) is not suited for computational purposes and therefore we use the approximation

$$(3.1) \quad \dot{I}(\tau_0)(I - I(\tau_0)) + \dot{U}(\tau_0)(U - U(\tau_0)) - (\tau - \tau_0) = 0$$

for τ sufficiently close to τ_0 assuming that $(U_0, I_0) := (U(\tau_0), I(\tau_0))$ and the unit tangent-vector $(\dot{U}_0, \dot{I}_0) := (\dot{U}(\tau_0), \dot{I}(\tau_0))$ are known.

Noting that I as given by (2.9) (for $i = i$) is a functional of z , i.e.

$I = I[z]$ we denote (3.1) by

$$(3.2) \quad N(z, U, \tau) = 0, \quad N : Z \times \mathbb{R}^2 \rightarrow \mathbb{R}$$

and augment $B(z, U) = 0$ by (3.2), that means we solve

$$(3.3) \quad P(y, \tau) = \begin{bmatrix} B(y) \\ N(y, \tau) \end{bmatrix} = 0, \quad y = (z, U)$$

where τ is in a sufficiently small neighborhood of τ_0 . We will show that the I - U -characteristic can be computed by solving (3.3) by continuation in τ (at least locally about τ_0) even if U_0 is a snap-back voltage.

A geometrical algorithm for the determination of $(U(\tau), I(\tau))$ as defined by (3.1) is as follows. At first the point S_0 on the tangent to (U_0, I_0) , whose distance to (U_0, I_0) is $|\tau - \tau_0|$ (if $\tau - \tau_0 > 0$ the vector pointing from (U_0, I_0) to S_0 is oriented as the tangent vector (\dot{U}_0, \dot{I}_0) and if $\tau - \tau_0 < 0$ it is oriented in the opposite direction) is determined. The normal to the tangent through S_0 is intersected with the characteristic curve giving $(U(\tau), I(\tau))$. This is illustrated in Figure 2 at a 'regular point' (a non-snap-back-point) of the characteristic.

Figure 3 demonstrates the reparameterization at a snap-back-point (U_0, I_0) . It is intuitively clear that $(U(\tau), I(\tau))$ can be determined in a locally unique way if $|\tau - \tau_0|$ is sufficiently small.

To prove this we define 'regular points' and 'simple limit points' (i.e. snap-back points) mathematically (see H. Keller (1977)).

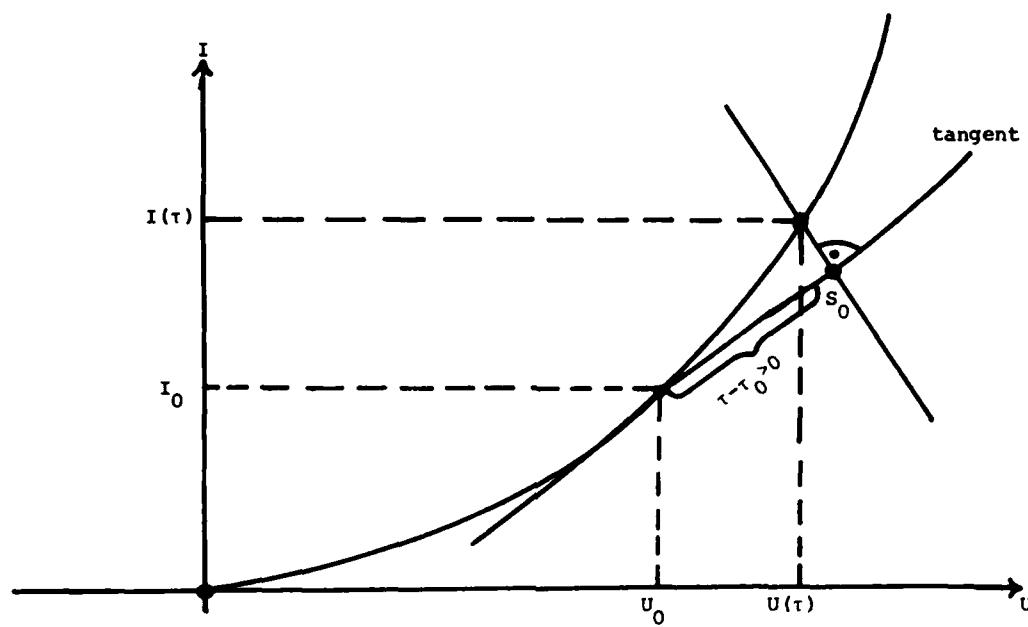


Figure 2. A Regular Point

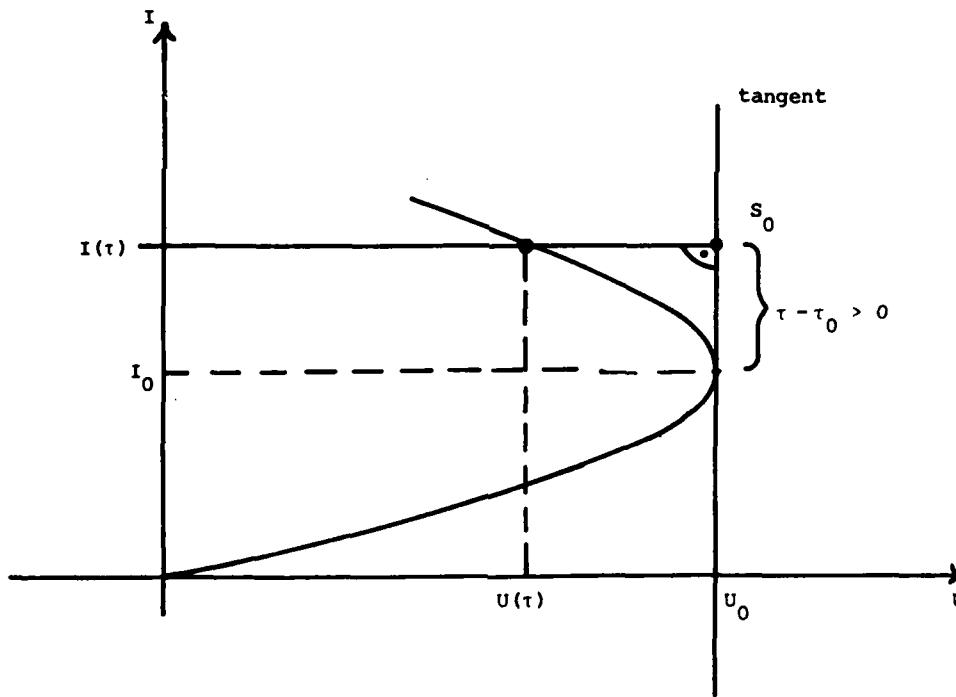


Figure 3. A 'Snap-back Point'

For the reader who is not familiar with the concepts of nonlinear analysis in Banach spaces we remark that, for understanding the implications of the following, it suffices to regard B as a function from \mathbb{R}^{K+1} into \mathbb{R}^K and N as a function from \mathbb{R}^{K+2} into \mathbb{R} for some integer K . Then Frechet derivatives (linearizations) are then Jacobi matrices of corresponding dimensions. This corresponds to analyzing an appropriate discretization of the semiconductor device equations (subject to the mentioned boundary conditions) and of (3.1).

We define:

- 1) The point (z_0, U_0) ($z_0 := z(z_0)$) is the solution of $B(z, U_0) = 0$ with $I_0 = I(z_0)$ is called regular solution point of $B(z, U) = 0$ if the Frechet derivative $\frac{\partial B}{\partial z}(z_0, U_0)$ is one-to-one and onto (i.e. invertible).
- 2) The point (z_0, U_0) is called normal limit solution point of $B(z, U) = 0$ if $N(\frac{\partial B}{\partial z}(z_0, U_0))$ is one dimensional ($N(A)$ denotes the null space of the operator A), the codimension of $R(\frac{\partial B}{\partial z}(z_0, U_0))$ is one ($R(A)$ denotes the range of the operator A) and if $\frac{\partial B}{\partial U}(z_0, U_0) \notin R(\frac{\partial B}{\partial z}(z_0, U_0))$.

The following Theorem is along the lines of Keller's (1977) Theorem 3.3.

Theorem 3.1: Let (z_0, U_0) be either a regular solution or a normal limit solution of $B(z, U) = 0$. If B is sufficiently smooth then for $(\tau - \tau_0)$ sufficiently small there exists a unique smooth arc of solutions $(z(\tau), U(\tau))$ of $B(z, U) = 0$ passing through (z_0, U_0) and fulfilling (3.3). The Frechet derivatives $\frac{\partial P}{\partial (z, U)}$ are one-to-one and onto along this arc.

Proof:

$$C_0 := \frac{\partial P}{\partial (z, U)}(z_0, U_0, \tau_0) = \begin{bmatrix} \frac{\partial B}{\partial z}(z_0, U_0) & \frac{\partial B}{\partial U}(z_0, U_0) \\ \dot{I}(\tau_0) \frac{\partial I}{\partial z}[z_0] & \dot{U}(\tau_0) \end{bmatrix}$$

holds. If (z_0, U_0) is a regular solution point of $B(z, U) = 0$, then $\frac{\partial B}{\partial z}(z_0, U_0)$ is one-to-one and onto. To show that $\frac{\partial P}{\partial (z, U)}(z_0, U_0, \tau_0)$ is one-to-one and onto it suffices to prove that

$$(3.4) \quad a_0 := \dot{U}(\tau_0) - \dot{I}(\tau_0) \frac{\partial I}{\partial z} [z_0] \left(\frac{\partial B}{\partial z} (z_0, u_0) \right)^{-1} \frac{\partial B}{\partial u} (z_0, u_0) \neq 0$$

holds (see Keller (1977), Lemma 2.8)). By differentiating $B(z, u) = 0$ with respect to s

we obtain at $s = \tau_0$

$$(3.5) \quad \frac{\partial B}{\partial z} (z_0, u_0) \dot{z}(\tau_0) + \frac{\partial B}{\partial u} (z_0, u_0) \dot{U}(\tau_0) = 0.$$

$\dot{U}(\tau_0) = 0$ implies $\dot{z}(\tau_0) = 0$ (because of the nonsingularity of $\frac{\partial B}{\partial z} (z_0, u_0)$) and

$\dot{I}(\tau_0) = \frac{\partial I}{\partial z} [z_0] \dot{z}(\tau_0) = 0$ follows which contradicts (2.13). Therefore $\dot{U}(\tau_0) \neq 0$ and

$$\left(\frac{\partial B}{\partial z} (z_0, u_0) \right)^{-1} \frac{\partial B}{\partial u} (z_0, u_0) = - \frac{\dot{z}(\tau_0)}{\dot{U}(\tau_0)}$$

holds. Inserting this into (3.4) gives

$$a_0 = \dot{U}(\tau_0) + \dot{I}(\tau_0) \frac{\partial I}{\partial z} [z_0] \frac{\dot{z}(\tau_0)}{\dot{U}(\tau_0)}.$$

Thus

$$a_0 \dot{U}(\tau_0) = \dot{U}^2(\tau_0) + \dot{I}^2(\tau_0) = 1 \Rightarrow a_0 \neq 0$$

and C_0 is one-to-one and onto.

Now let (z_0, u_0) be a normal limit solution of $B(z, u) = 0$, (3.5) implies

$$\frac{\partial B}{\partial z} (z_0, u_0) \dot{z}(\tau_0) = - \frac{\partial B}{\partial u} (z_0, u_0) \dot{U}(\tau_0) = 0$$

because $\frac{\partial B}{\partial u} (z_0, u_0) \notin R(\frac{\partial B}{\partial z} (z_0, u_0))$. Since $\frac{\partial B}{\partial u} (z_0, u_0)$ is not the null-operator $\dot{U}(\tau_0) = 0$ follows (compare to Figure 3). Therefore $N(\frac{\partial B}{\partial z} (z_0, u_0)) = \text{span}\{\dot{z}(\tau_0)\}$

holds. Keller's (1977) Lemma 2.8 implies that C_0 is one-to-one and onto iff

$$(3.6) \quad \dim R(\dot{I}(\tau_0) \frac{\partial I}{\partial z} [z_0]) = 1$$

$$(3.7) \quad \dot{I}(\tau_0) \frac{\partial I}{\partial z} [z_0] \in N(\frac{\partial B}{\partial z} (z_0, u_0))$$

hold. Obviously

$$\dot{I}(\tau_0) \frac{\partial I}{\partial z} [z_0] \dot{z}_0 = \dot{I}^2(\tau_0) = 1$$

holds because of (2.13) ($\dot{U}(\tau_0) = 0$) and (3.6), (3.7) follow.

The invertibility of C_0 and the implicit function theorem (see Schwartz (1969)) imply Theorem 3.1. \square

The Theorem implies that - at least for $|\tau - \tau_0|$ sufficiently small - the solution arc of $B(z, U) = 0$ can be computed by solving (3.3) (which is the 'reparameterized version of $B(z, U) = 0$) for z and U (by continuation in τ) using Newton's method which is quadratically convergent along the whole solution arc.

4. Implementation

For the numerical solution of the fundamental semiconductor device equations $B(z, U) = 0$ the problem has to be discretized appropriately, that means $B_h(z_h, U) = 0$ has to be solved instead of $B(z, U) = 0$ (h represents the grid parameter). For a collection of results on discretization methods see Mock (1983).

We now assume that B_h has already been chosen and that $B_h : \mathbb{R}^{K+1} \rightarrow \mathbb{R}^K$. Also an appropriate numerical integration rule $I_h[z_h]$ has to be used to discretize

$$I[z] = \int_C I \cdot nds.$$

To get the continuation started at $S = S_0$ we solve $B_h(z_h, U_0) = 0$ obtaining z_{h_0} (we assume that $(z_{h_0}, U_0) =: (z_h(\tau_0), U(\tau_0))$ is a regular solution of $B(z, U) = 0$) and $(I_{h_0} := I_h[z_{h_0}])$. An approximation of the tangent vector to the $I - U$ characteristic at (U_0, I_0) can be obtained by solving $B_h(z_h, \tilde{U}_0) = 0$ (with $\Delta U_0 = \tilde{U}_0 - U_0$ suff. small) for $z_h = \tilde{z}_{h_0}$ and by setting

$$\dot{\tilde{U}}_0 = \frac{\tilde{U}_0 - U_0}{\omega}, \quad \dot{I}_0 = \frac{I_h[\tilde{z}_{h_0}] - I_h[z_{h_0}]}{\omega}$$

$$\text{with } \omega = \sqrt{(\tilde{U}_0 - U_0)^2 + (I_h[\tilde{z}_{h_0}] - I_h[z_{h_0}])^2}.$$

Assume now that we already solved

$$(4.1) \quad N_h(z_h, U_h, \tau) \equiv \begin{bmatrix} B_h(z_h, U_h) \\ N(z_h, U_h, \tau) \end{bmatrix} = 0$$

for $\tau = \tau_K$ (i.e. $(z_h(\tau_K), U_h(\tau_K))$ and $I_h(\tau_K)$ are known). We compute

$$(z'_h(\tau_K), U'_h(\tau_K)) := \left(\frac{d}{d\tau} z_h(\tau_K), \frac{d}{d\tau} U_h(\tau_K) \right) \text{ from}$$

$$(4.2) \quad \frac{d}{d\tau} N_h(z_h, U_h, \tau_K) = \begin{bmatrix} \frac{\partial B_h}{\partial z}(z_h(\tau_K), U_h(\tau_K)) \frac{\partial B_h}{\partial U}(z_h(\tau_K), U_h(\tau_K)) \\ \dot{I}(\tau_0) \frac{\partial I_h}{\partial z_h}[z_h(\tau_K)] & \dot{U}(\tau_0) \end{bmatrix} \begin{bmatrix} \dot{z}_h(\tau_K) \\ \dot{U}(\tau_K) \end{bmatrix} + \begin{bmatrix} 0 \\ -1 \end{bmatrix} = 0$$

and obtain $I'_h(\tau_K) = \frac{\partial I_h}{\partial z_h} [z_h(\tau_K)] z'_h(\tau_K)$. For the continuation we choose $\Delta\tau_K$, set $\tau_{K+1} = \tau_K + \Delta\tau_K$ and solve (4.1) for $\tau = \tau_{K+1}$. As initial guess for the iteration procedure for the numerical solution of (4.1) we pick the Euler predictor

$$(4.3) \quad \begin{pmatrix} z_h^{(0)}(\tau_{K+1}) \\ u_h^{(0)}(\tau_{K+1}) \end{pmatrix} = \begin{pmatrix} z_h(\tau_K) \\ u_h(\tau_K) \end{pmatrix} + \Delta\tau_K \begin{pmatrix} z'_h(\tau_K) \\ u'_h(\tau_K) \end{pmatrix}.$$

If the I-U-characteristic consists only of regular and limit points then it follows from Keller (1975) and from Theorem 3.1 (we assume that τ_{K+1} is suff. close to τ_0 such that Theorem 3.1 holds for $\tau = \tau_{K+1}$) that Newton's method converges quadratically if $\Delta\tau_K$ is sufficiently small, and if P_h is a stable and consistent (see Keller (1975)) approximation to P .

Since Theorem 3.1 implies that $\frac{\partial P}{\partial (z, U)} (z(\tau), U(\tau), \tau)$ is nonsingular if $|\tau - \tau_0|$ is suff. small it is recommendable to update τ_0 (and N) after a few continuation steps. This is done by setting:

$$(4.4)(a) \quad \tau_0^{(NEW)} := \tau_{k+1}$$

and

$$(4.4)(b) \quad (\dot{U}(\tau_0^{(NEW)}), \dot{I}(\tau_0^{(NEW)})) := \frac{(U'(\tau_{k+1}), I'(\tau_{k+1}))}{\sqrt{(U'(\tau_{k+1}))^2 + (I'(\tau_{k+1}))^2}}.$$

A way to determine when an update is desirable is to require that the length of the tangent vector $(U'(\tau_K), I'(\tau_K))$ differs from 1 by less than a certain prescribed error tolerance.

Of course, the sign of the increments $\Delta\tau_K$ has to be constant throughout the whole continuation process (and equal to the sign of ΔU_0). For the thyristor characteristic with $U_0 = I_0 = 0$, $\tau_0 = 0$ positive increments ($\Delta U_0 > 0, \Delta\tau_K > 0$) imply that one 'walks up' the forward characteristic ($U > 0$) and negative increments ($\Delta U_0 < 0, \Delta\tau_K < 0$) result in the computation of the reverse characteristic ($U < 0$).

The increments $\Delta\tau_K$ have to be chosen such that the initial guess (4.3) lies in the domain of attraction of the iteration method for (4.1) at $\tau = \tau_{K+1}$. For a sufficiently smooth solution arc

$$(4.5) \quad \begin{pmatrix} z_h(\tau_{K+1}) \\ u_h(\tau_{K+1}) \end{pmatrix} - \begin{pmatrix} z_h^{(0)}(\tau_{K+1}) \\ u_h^{(0)}(\tau_{K+1}) \end{pmatrix} = \frac{(\Delta\tau_K)^2}{2} \begin{pmatrix} z_h''(\xi_K) \\ u_h''(\xi_K) \end{pmatrix}, \quad \xi_K \in (\tau_K, \tau_{K+1})$$

holds. Therefore one has to require that

$$(4.6) \quad |\Delta\tau_K| \lesssim [(2|z_h''|_{[\tau_K, \tau_{K+1}]} + 2|u_h''|_{[\tau_K, \tau_{K+1}]})\delta_{K+1}]^{\frac{1}{2}}$$

where δ_{K+1} represents the convergence radius of the iterative method for the approximate solution of (4.1) at $\tau = \tau_{K+1}$. Computable estimates for δ_{K+1} and strategies slightly different from (4.6) can be found in Den Heijer and Rheinboldt (1981).

Assume now that a Newton-type procedure is used as iteration-method. Then a linear system of the form

$$(4.7) \quad \begin{pmatrix} A_h & b_h \\ c_h & d \end{pmatrix} \begin{pmatrix} \delta z_h \\ \delta u_h \end{pmatrix} = \begin{pmatrix} v_h \\ w_h \end{pmatrix}$$

has to be solved at every iteration step (and also for solving (4.2)) with

$$(4.8) \quad \left. \begin{array}{l} A_h = \frac{\partial B_h}{\partial z_h} \\ b_h = \frac{\partial B_h}{\partial u} \\ c_h = \frac{\partial N_h}{\partial z_h} \\ d = \frac{\partial N_h}{\partial u} \end{array} \right\} \text{evaluated at some iterate } (z_h^{(k)}, u_h^{(k)}) \text{ and } \tau = \tau_K.$$

If a Gauss-solver for sparse matrices is used to solve systems of the form $A_h z_h = r_h$ (which occur in solving the fundamental semiconductor device equations (2.10) for prescribed ϕ - V -voltages) then it can easily be modified to solve systems of the form (5.7). The $K + 1$ -st row $\begin{pmatrix} b_h \\ d \end{pmatrix}$ and the $K + 1$ -st column (c_h, d) do not create additional fill-in during the elimination process.

If a band-solver is used to solve systems with coefficient matrices A_h then systems of the form (4.7) can be solved as suggested in Keller (1977), that is by solving two systems with coefficient matrix A_h simultaneously. This, of course, only gives accurate results when A_h has a moderate condition number, i.e. when τ_K does not correspond to a limit point. However, it is possible to continue beyond limit points when using the parameterization (3.1) (see Keller (1977), Theorem 4.4).

5. A Test Problem

As a test problem we applied the arclength-continuation procedure to the one-dimensional semiconductor device equations modelling a silicon pn-junction in the avalanche case.

For simplicity we took an odd, piecewise continuous doping profile (see Figure 4).

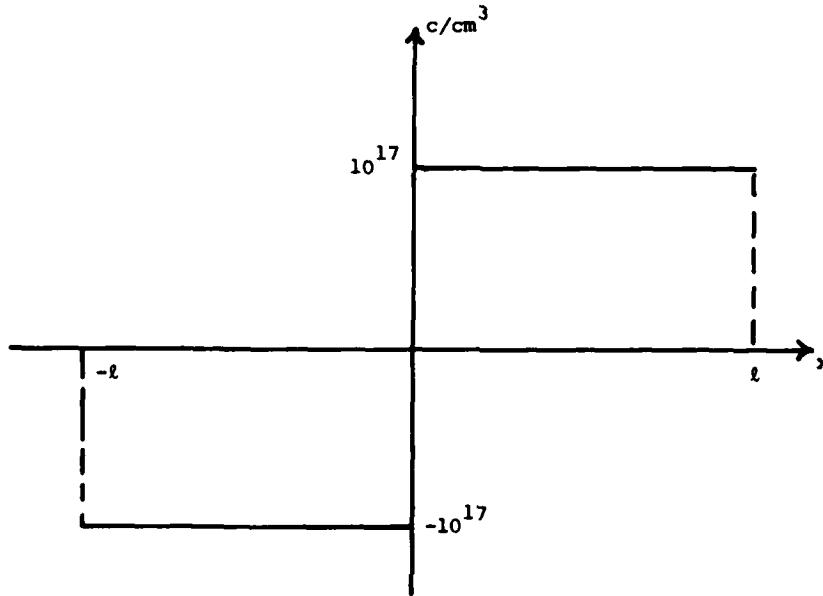


Figure 4. Doping Profile

The length of the pn-junction is $2l = 5 \times 10^{-3} \text{ cm}$.

The avalanche phenomenon was modelled by the generation rate

$$(5.1) \quad R = -\alpha(\psi')(|J_n| + |J_p|)$$

with J_n, J_p given by (2.4), (2.5) resp. The following expression was used for the hole and electron ion isolation rate:

$$(5.2) \quad \alpha(\psi'(x)) = \sigma_1 \exp\left(-\frac{\sigma_2}{|\psi'(x)|}\right); \sigma_1, \sigma_2 > 0.$$

The electron and hole mobilities were taken equal (also the electron and hole diffusivities). The obtained results should not be regarded as physically significant, they however illustrate very well the power of the reparameterization technique.

We remark that in the one-dimensional case the current is constant and given by

$$(5.3) \quad I \equiv q(D_n(n' - p') - \mu_n(n + p)\psi') \quad (\text{for } D_n = D_p, \mu_n = \mu_p).$$

A scaled version of (2.1)-(2.3) (see Markowich (1983a) for the scaling) was discretized by using the three-point-scheme for Poisson's equation and the Scharfetter-Gummel scheme for the continuity equations (see Markowich *et al.* (1983)).

The functional $I_h(z_h)$ was obtained by discretizing the current (5.3) at the largest grid point x_1 with $x_1 < 1$ also using the Scharfetter-Gummel discretization.

Figure 5 shows the obtained I-U-characteristic for $-5U_T < U < 0$ (U_T is the thermal voltage). The onset of avalanche generation occurs at $U = -1.5U_T$ and the current increases linearly (in absolute value) beyond that. This linear increase continues as far as $U = -200U_T$. Then the increase gets faster and the snap-back occurs at $U = -240U_T$ (see Figure 6). The continuation of the solution arc beyond the limit point was no problem.

Figures 7 and 8 show $\int_{-1}^1 a(\psi'(s))ds$ over the applied bias. For $U = 0$ (equilibrium solution) $\int_{-1}^1 a(\psi')ds < 1$, then it increases until it equals 1. This happens around that U -value at which avalanche generation starts, i.e. $U = -1.5U_T$ (compare to Figure 5). Then $\int_{-1}^1 a(\psi')ds$ remains almost constant until close to the snap-back voltage (see Figure 4). Slightly before the snap-back voltage it increases and gets significantly larger than 1. It was often claimed (see, for example, Sze (1981)) that 'breakdown' happens at that voltage at which $\int_{-1}^1 a(\psi')ds$ reaches one. This is not true in the mathematical sense for our simple model, there is a continuous branch of solutions (of the one-dimensional semiconductor problem in the case of avalanche generation) which emerges at the equilibrium solution (for $U = 0$) and which contains at least one solution for every $U < 0$ (see Markowich (1983b)). The situation, however, might change if temperature is introduced as unknown quantity.

J-U-CHARACTERISTIC

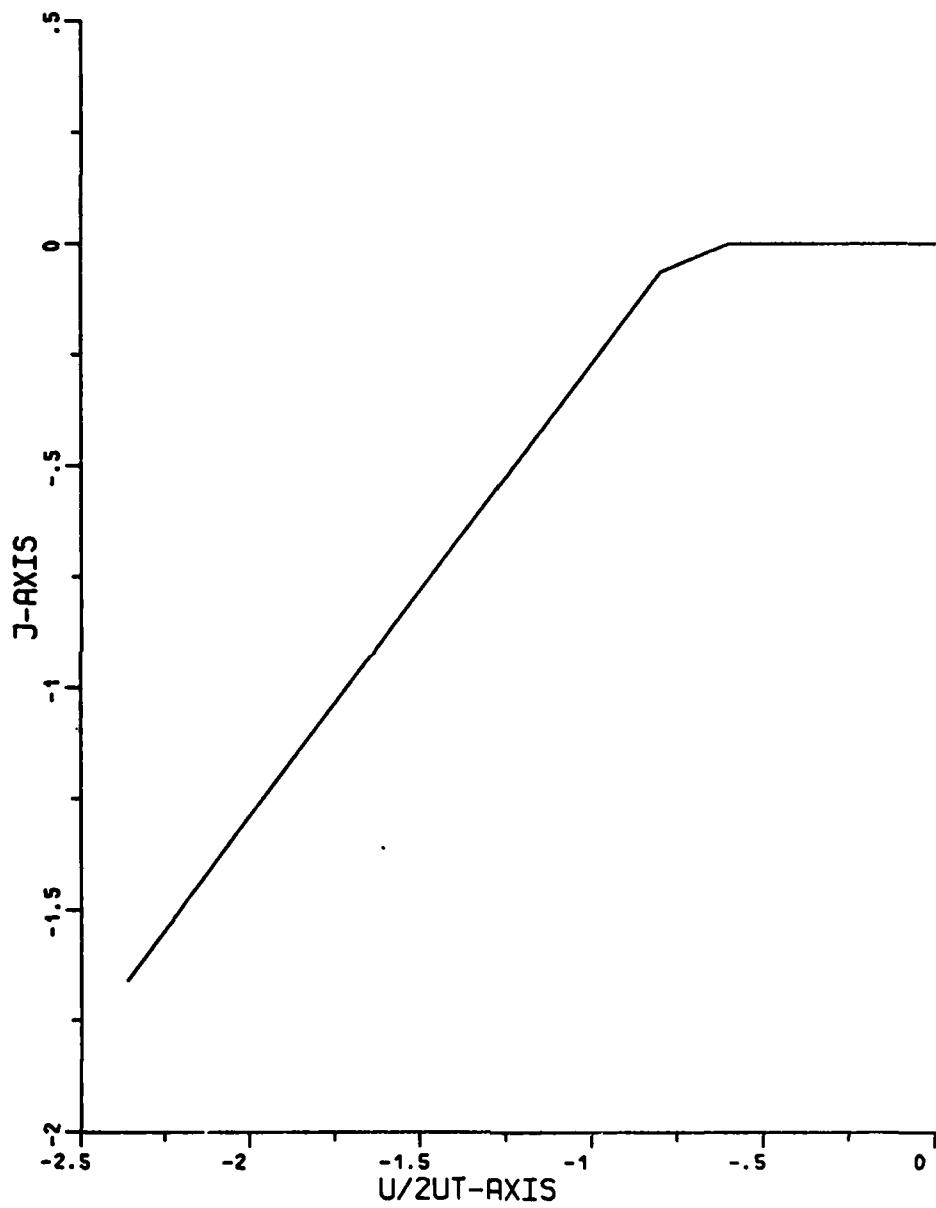


Figure 5

J-U-CHARACTERISTIC

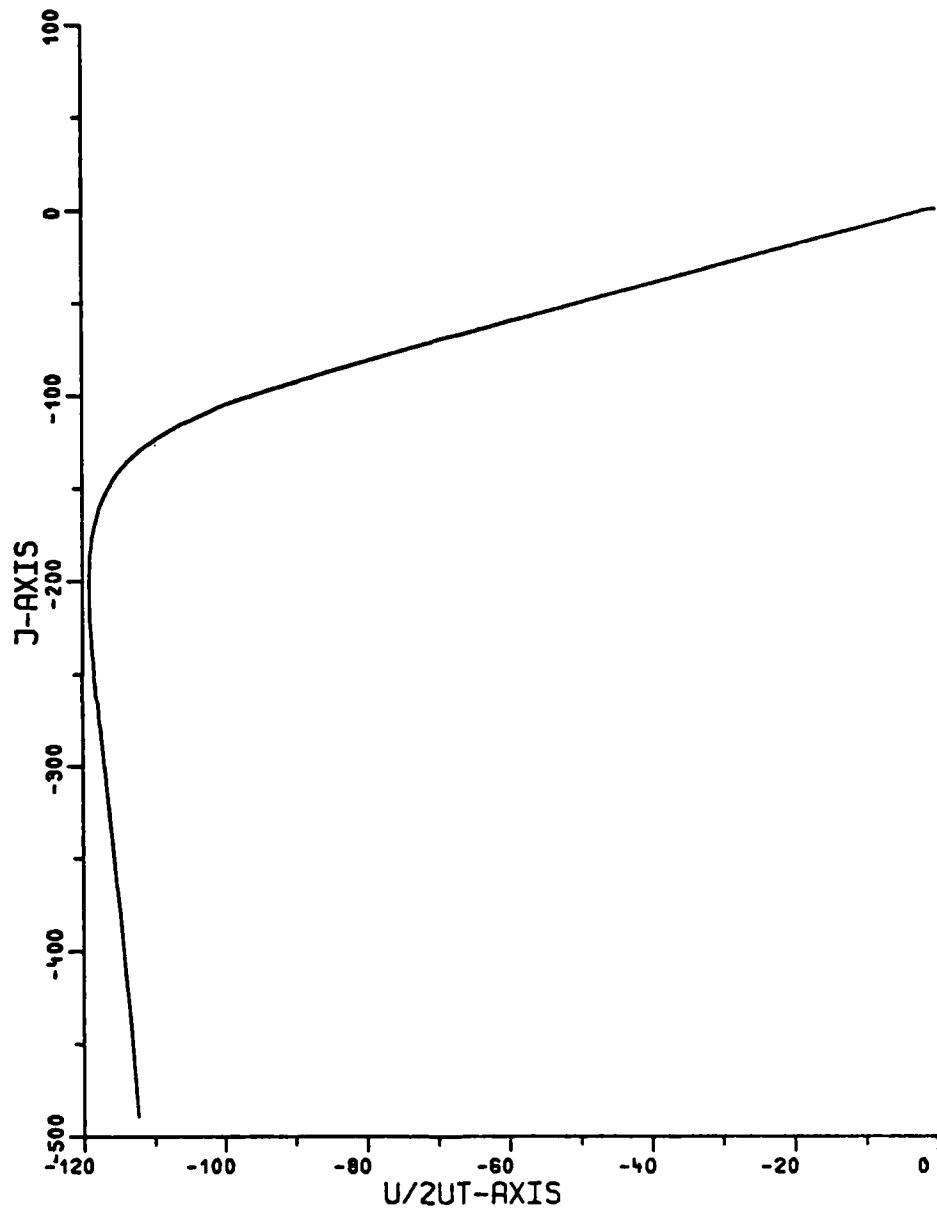


Figure 6

INT(ALPHA)
OVER APPLIED BIAS

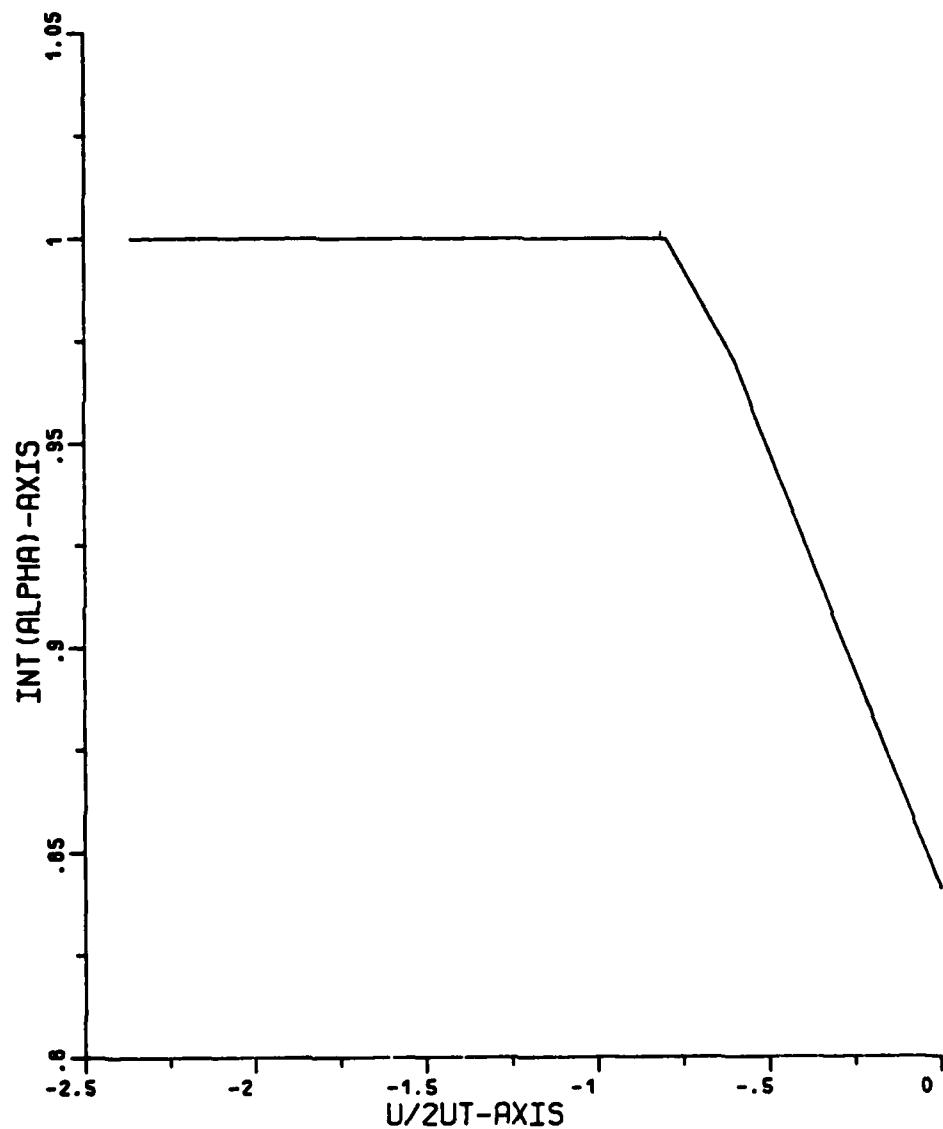


Figure 7

INT(ALPHA)
OVER APPLIED BIAS

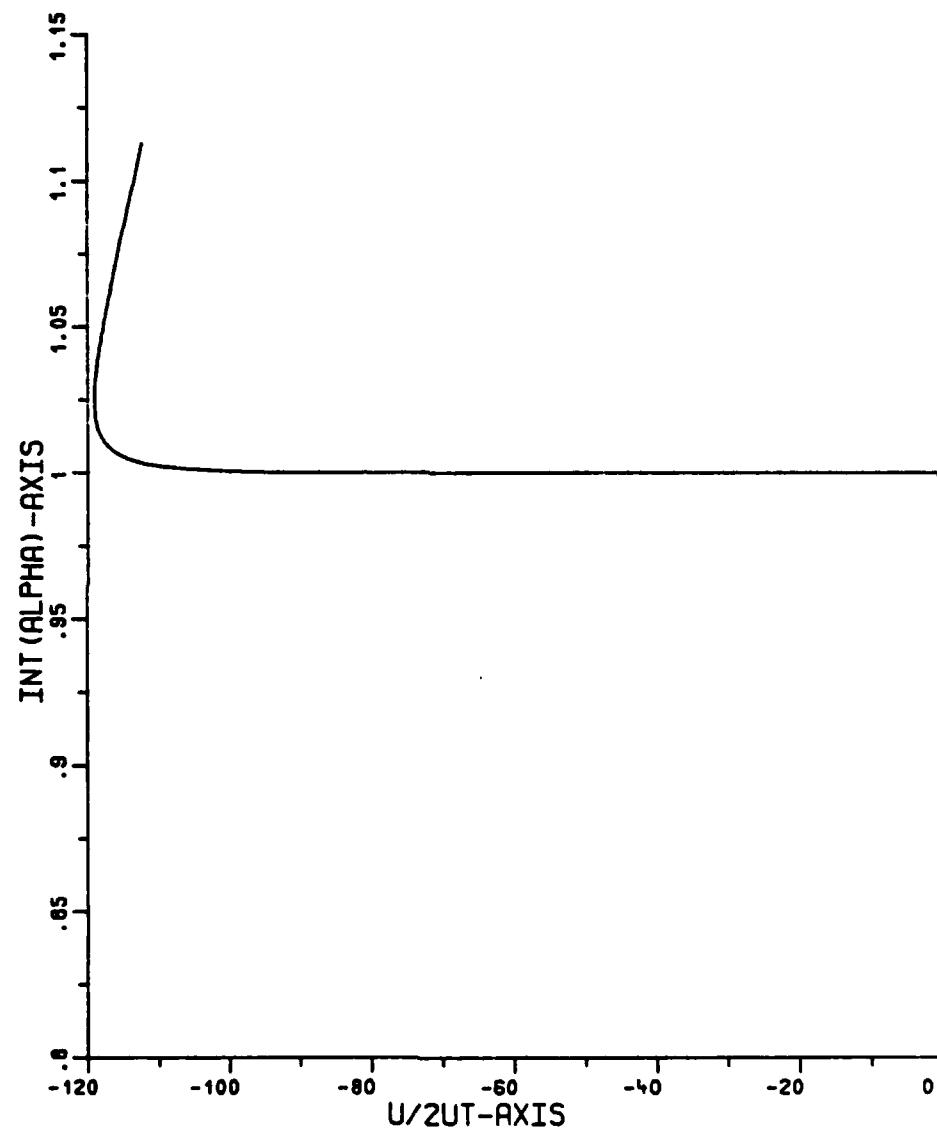


Figure 8

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This paper is concerned with the computation of semiconductor device current-voltage characteristics. We describe an algorithm which allows the computation of characteristics by continuation in a parameter which approximates the arclength of the characteristic. The use of this parameterization allows the characteristic to continue beyond snap-back-voltages, while continuation in the voltage fails past snap-back-voltages. We discuss the implementation of the parameterization and give a numerical example.		

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